



Twin Cities ANSYS® User Meeting

November 2011

Mesh Discretization Error





Mesh Discretization Error

1. Mesh Discretization: The “One-sided” Error Source
2. Tet Pregidous
3. Case Study A: Shape-Functions Effect
 - With and without mid-side nodes
 - Stresses & Deflection
4. Case Study B: Mesh Convergence
 - Node vs. Element (Averaged vs Unaveraged)
 - PRERR (SEPC/SMXB)

Mesh Discretization Error



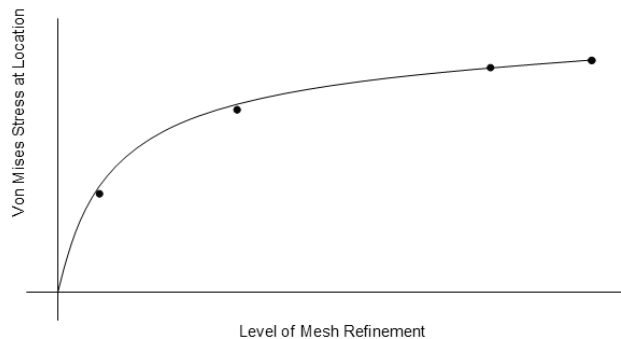
- Often small compared to load/material property error/scatter
- Ownership of error lands on analyst
 - Often linked to “credibility” of whole analysis
- True Error analysis would likely show Mesh Discretization is minor issue
 - And yet... Scrutiny continues
 - And rules and criteria abound... (while other scatter goes unmentioned)

“It can be *measured*? Well let’s fixate on it!”

Mesh Discretization Error



- A “one-sided” error source*
 - Predictions are usually **lower** than actual (not higher)
 - Excepting Singularities
 - Nagging feeling because of non-conservative nature
 - Stress is usually underpredicted*
 - Upper bound not determinable
 - Without employing knowledge of materials/loads/element shape functions – discussed later



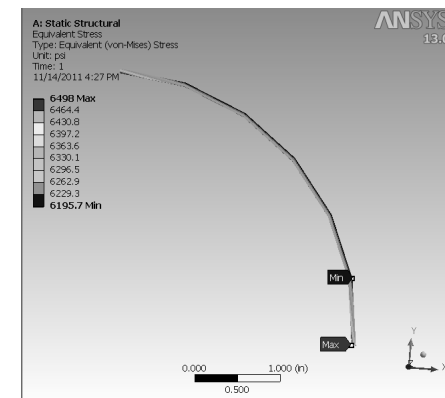
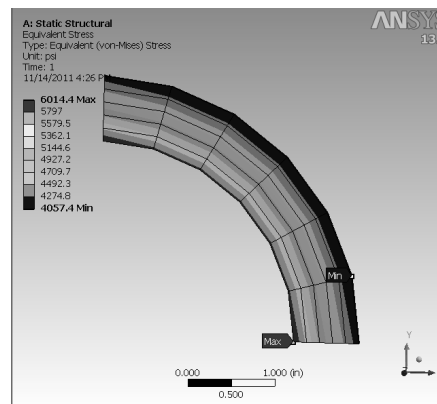
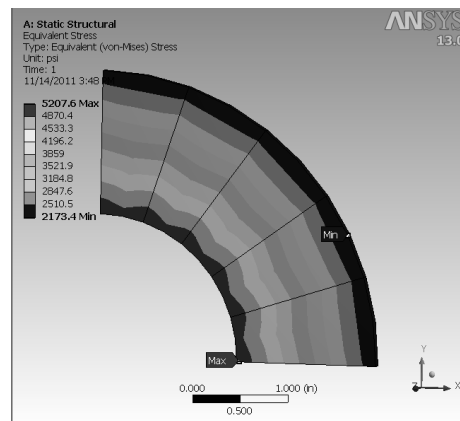
*Powergraphics results (classic)
isn't so one-sided – discussed later

- Bias Against Tetrahedrons (Tet's)
 - Source of grievance?
 - Low order Tets (a.k.a "T4", a.k.a "non-midside noded Tet")
 - Too Stiff in bending / large error with 1 element through thickness
 - 1st Tet's (Berkely 1960's) were high order
 - You'd have to work at it to get ANSYS to create T4's (structural)
 - Tets (10 noded) are Less efficient per DOF
 - Longer solve times
 - Shorter meshing times
 - Added control allows refinement at location of interest
 - **More** efficient than Mapped meshing!
 - Less pleasing to the eye (esp. higher aspect ratios)
 - Stigmatism is receding over last decade

Case Study A



- Thick to thin rings with inner pressfit (radial expansion)
 - Stress gradient related to radius^2
- Case Study A, Expansion of Thick/Thin Ring
 - Actually used 5° wedge

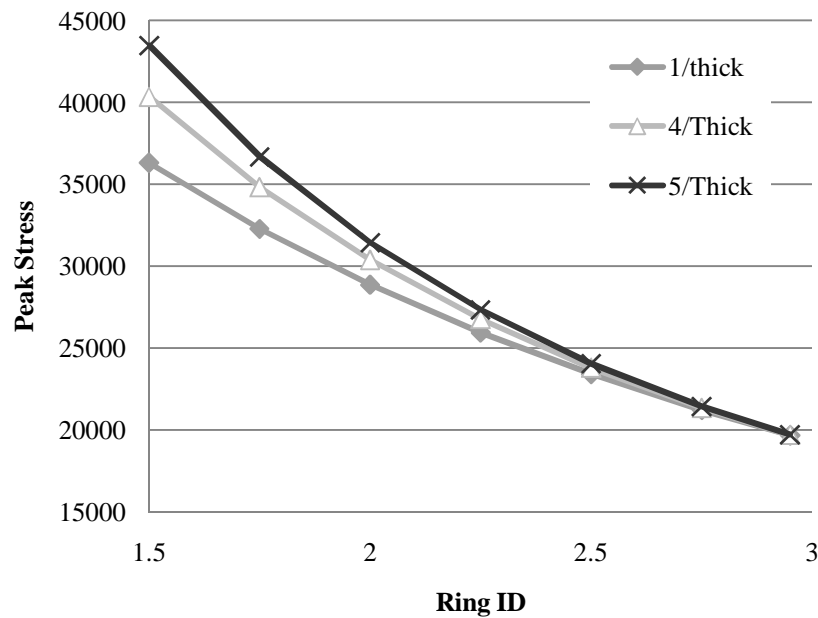


Case Study A

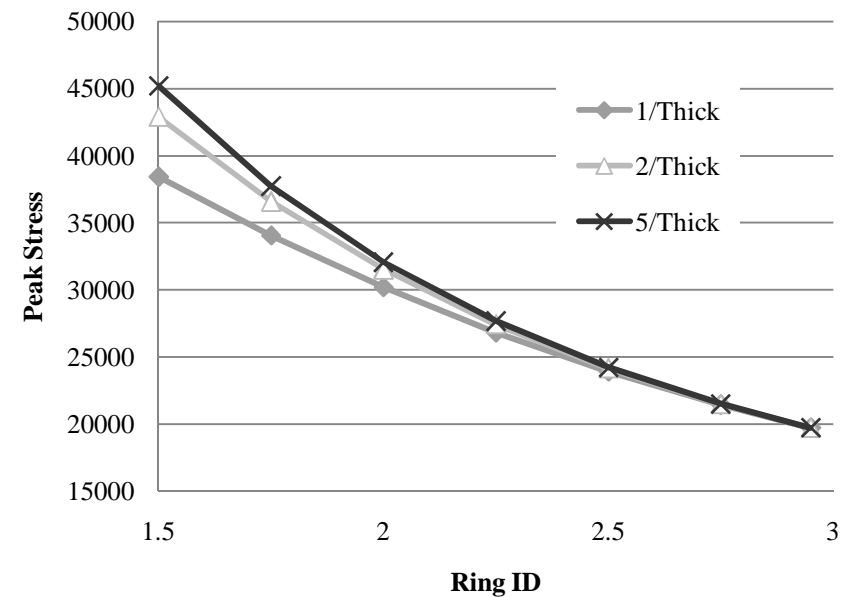


- Case Study A
 - Peak Stresses have similar convergence patterns/rate

Low Order Elements



High Order Elements

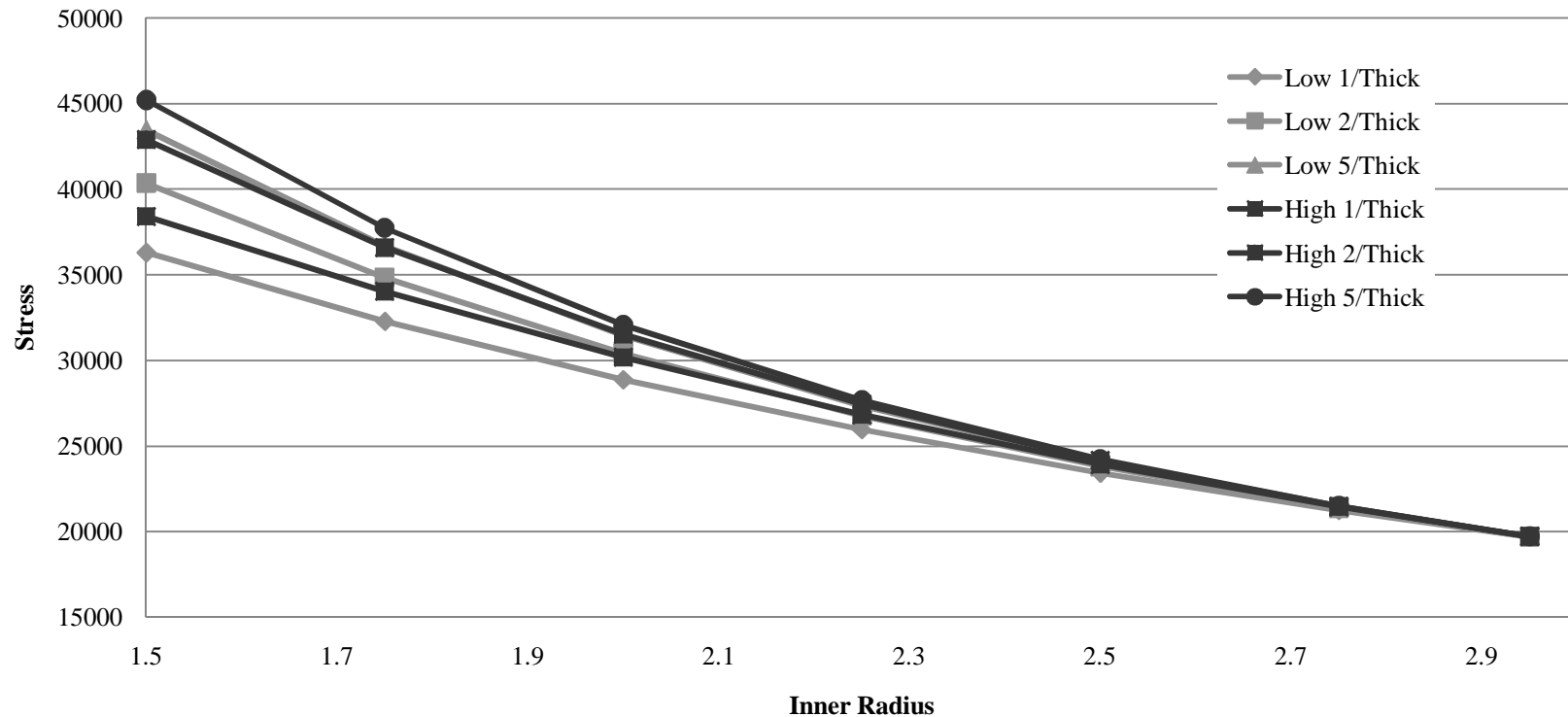


Case Study A



- Case Study A
 - Peak Stresses have similar convergence patterns/rate

High & Low Order Elements

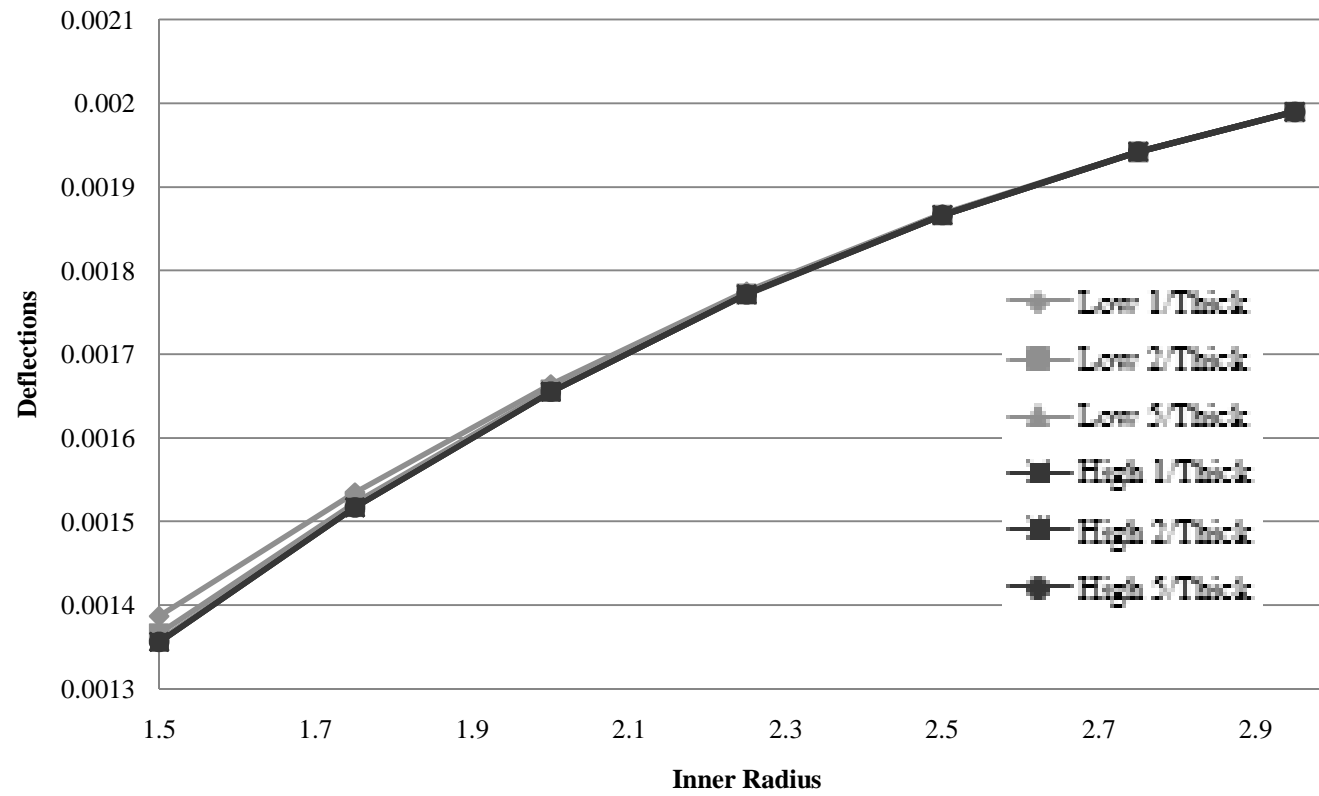


Case Study A



- Case Study A
 - OD Deflections

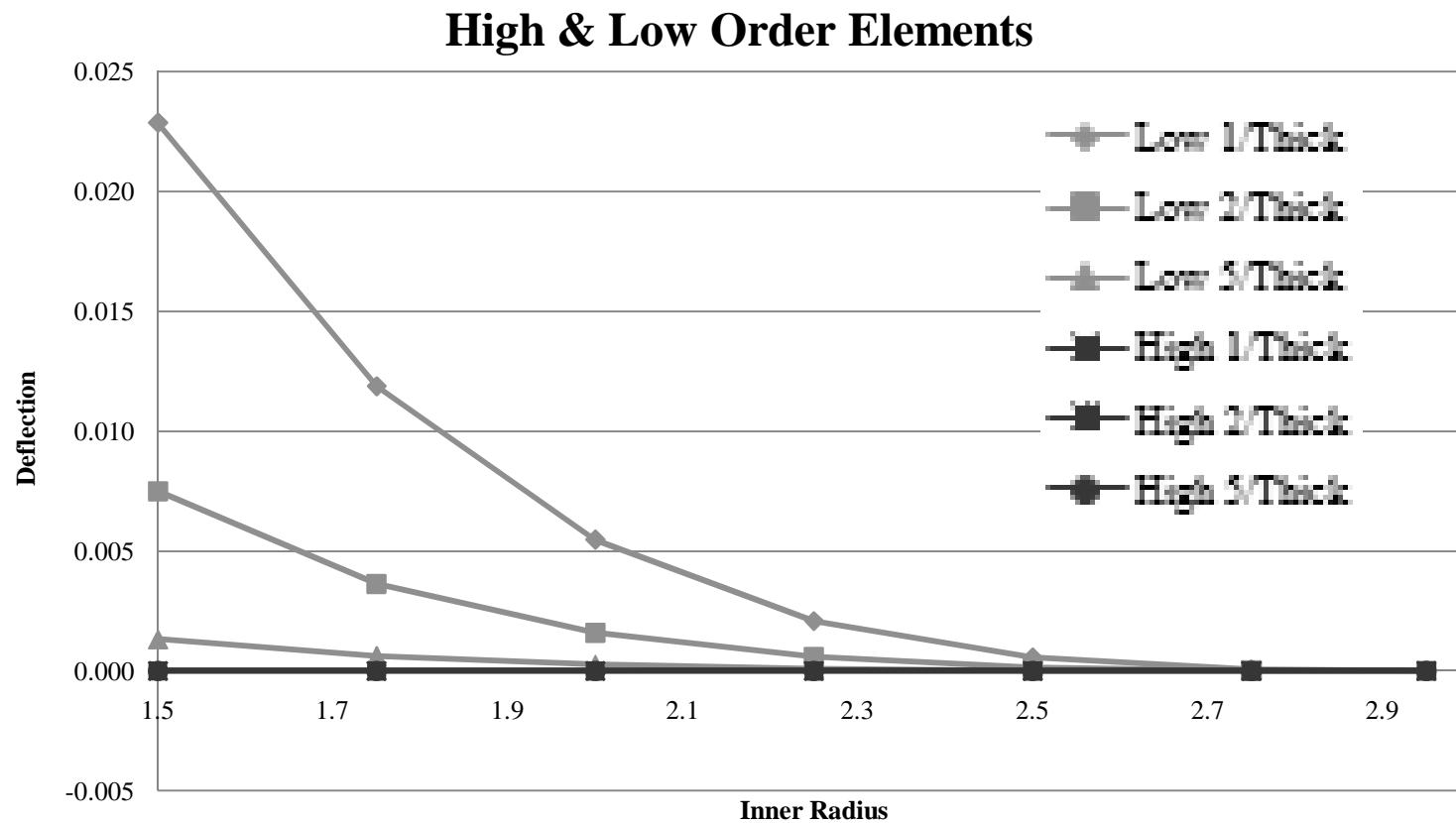
High & Low Order Elements



Case Study A



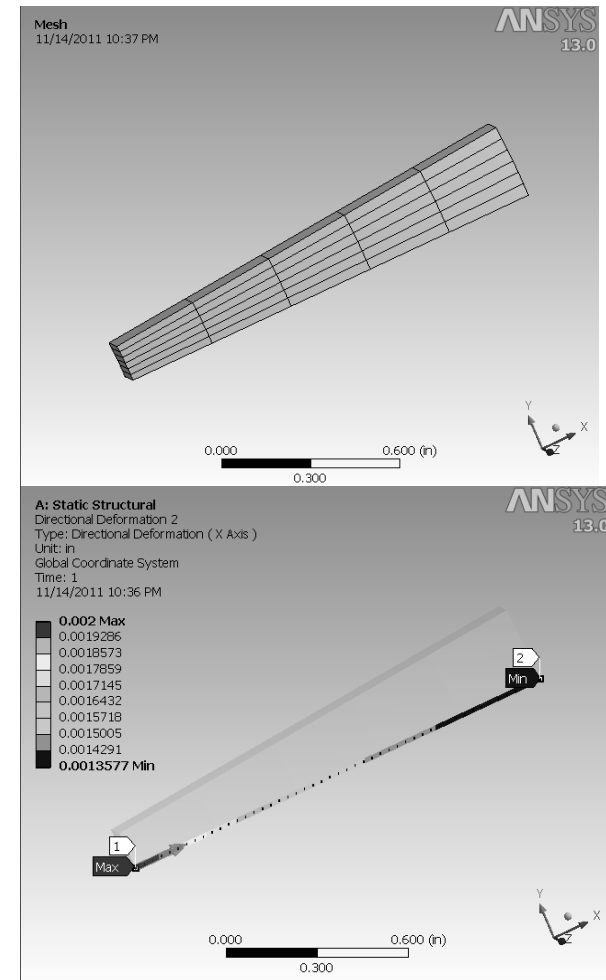
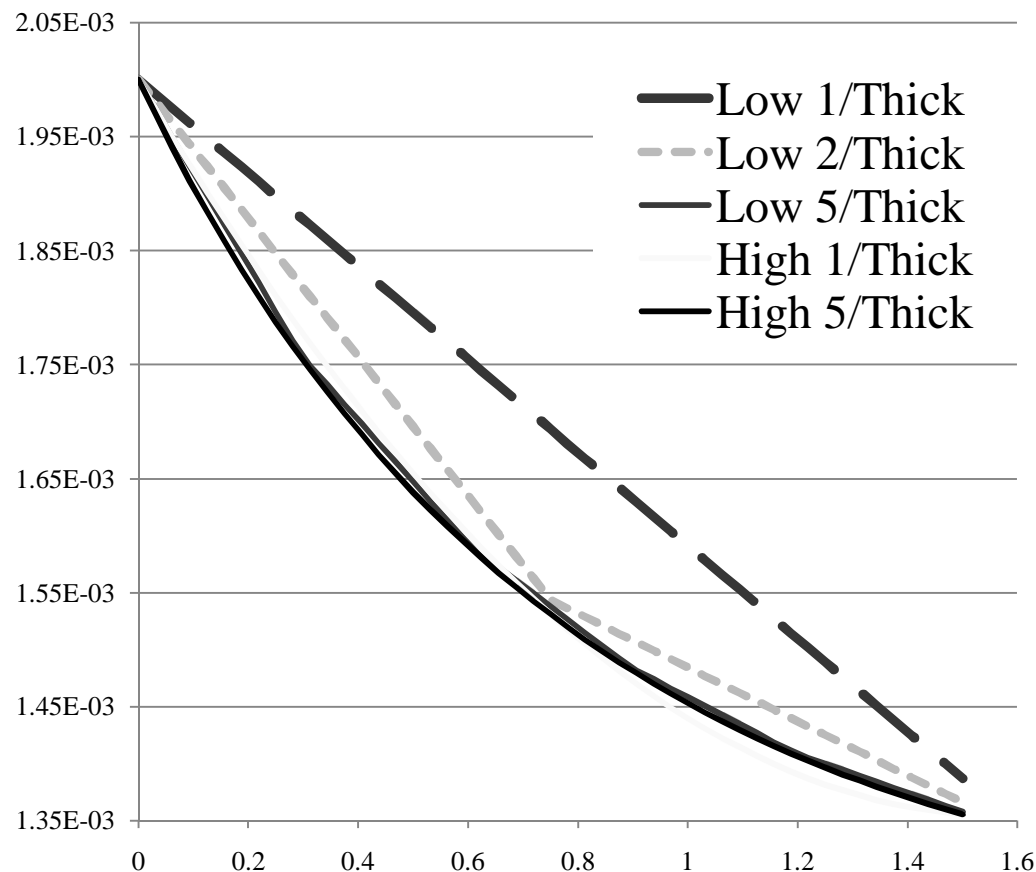
- Case Study A
 - OD Deflections



Case Study A



- Case Study A
 - Deflections Along Path

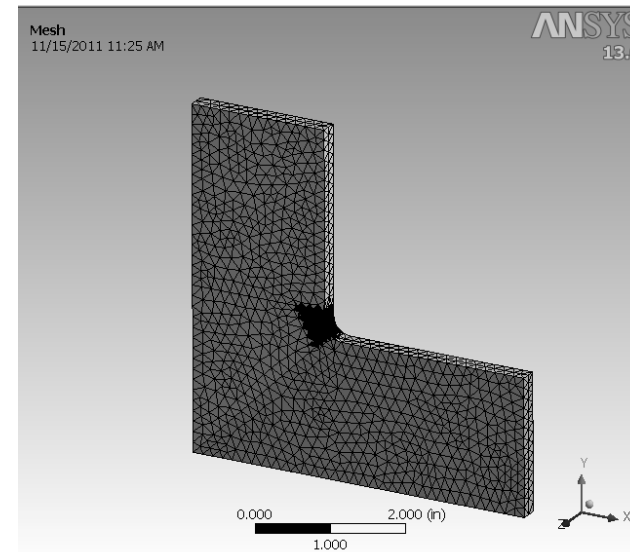
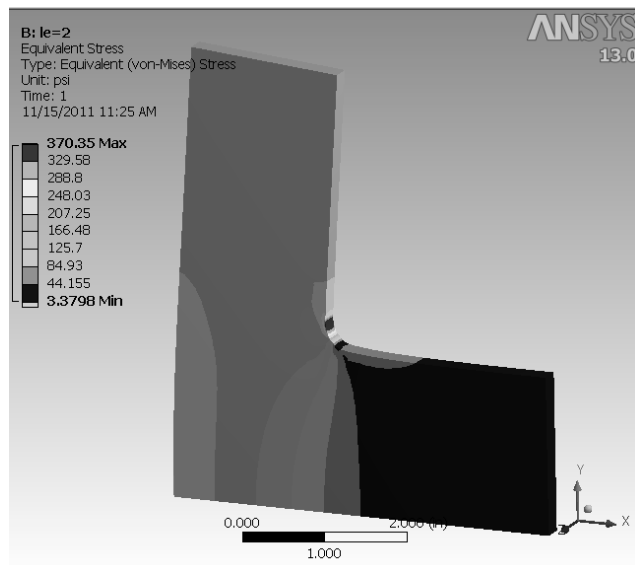


- Case Study A Conclusions
 - Element Stress Gradient
 - Linear for high or low order elements
 - Element Displacement Gradient
 - Linear for low order element
 - 2nd order polynomial for high order element
 - Thin Rings are well approximated with single element through the thickness
 - This extends to beams as well

Mesh Discretization Error



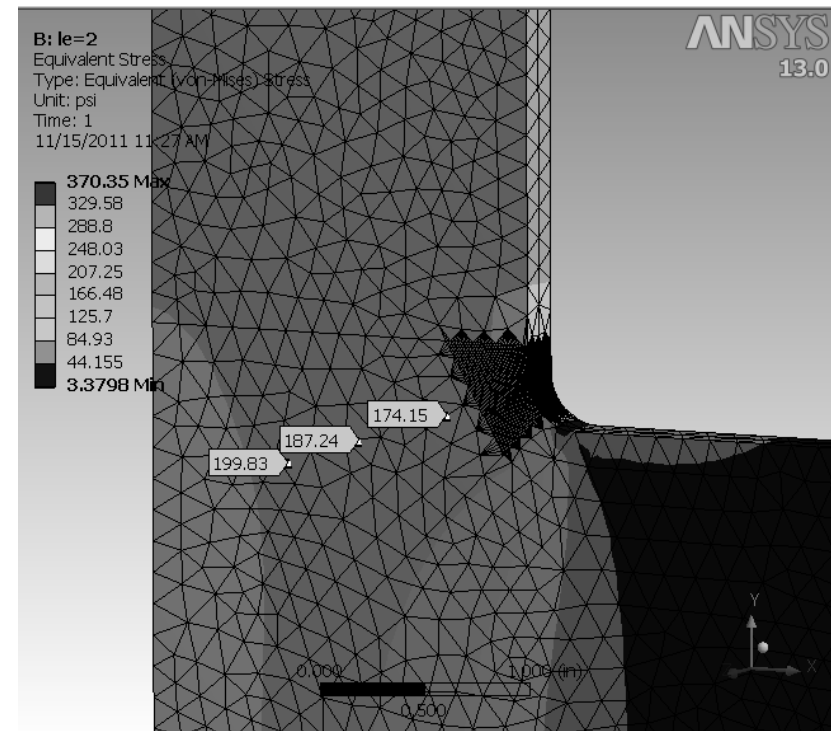
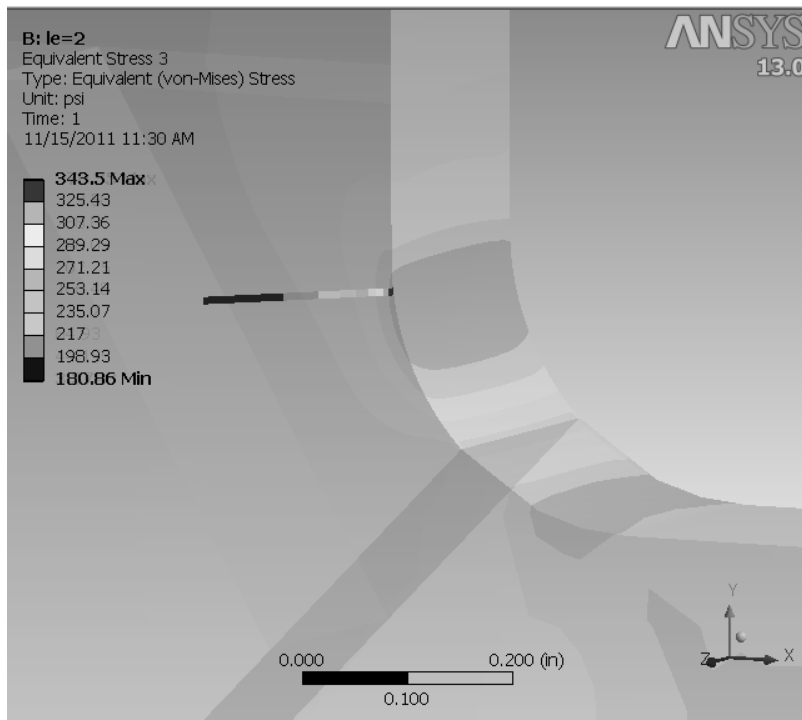
- Case Study B
 - Stress along path
 - Node vs. Element (Averaged vs Unaveraged)
 - PRERR (SEPC/SMXB)



Case Study B



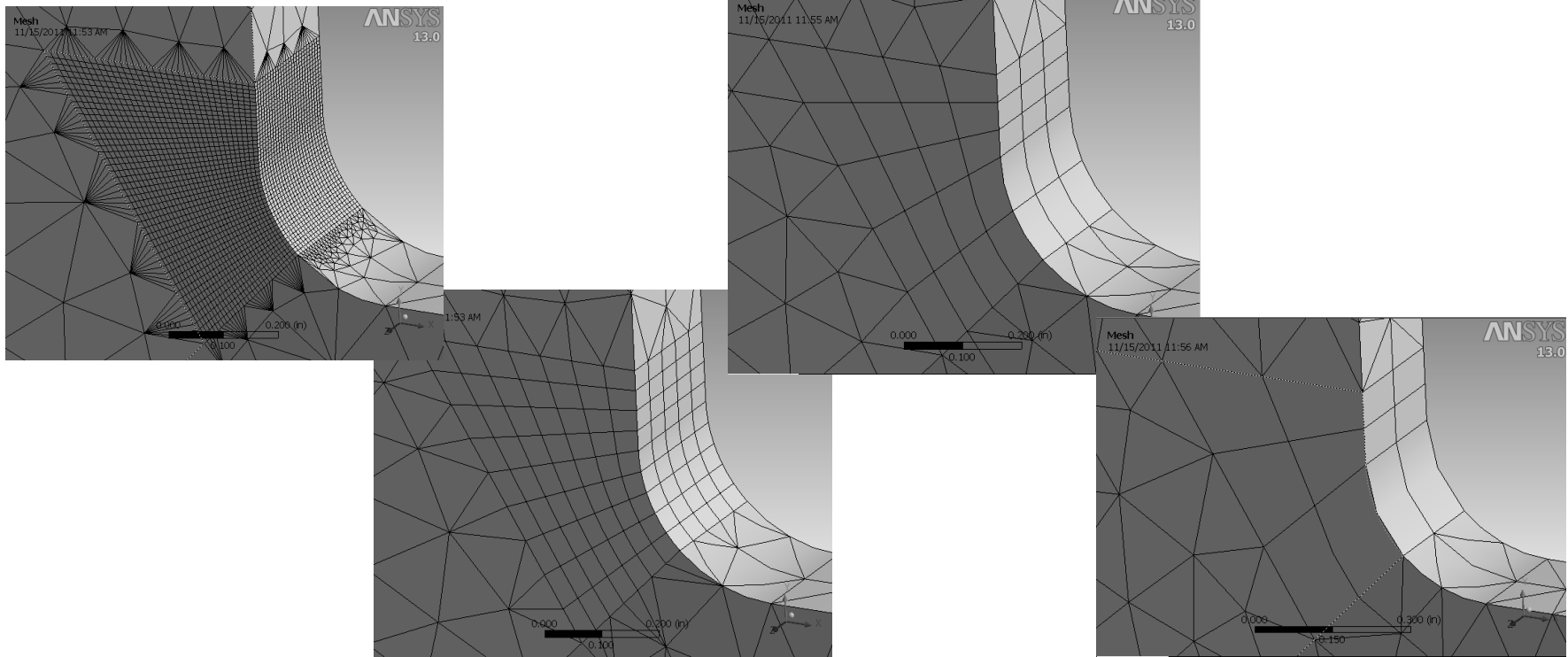
- Stress along path
 - Background stress of 180
 - $KT = 2.0$



Case Study B



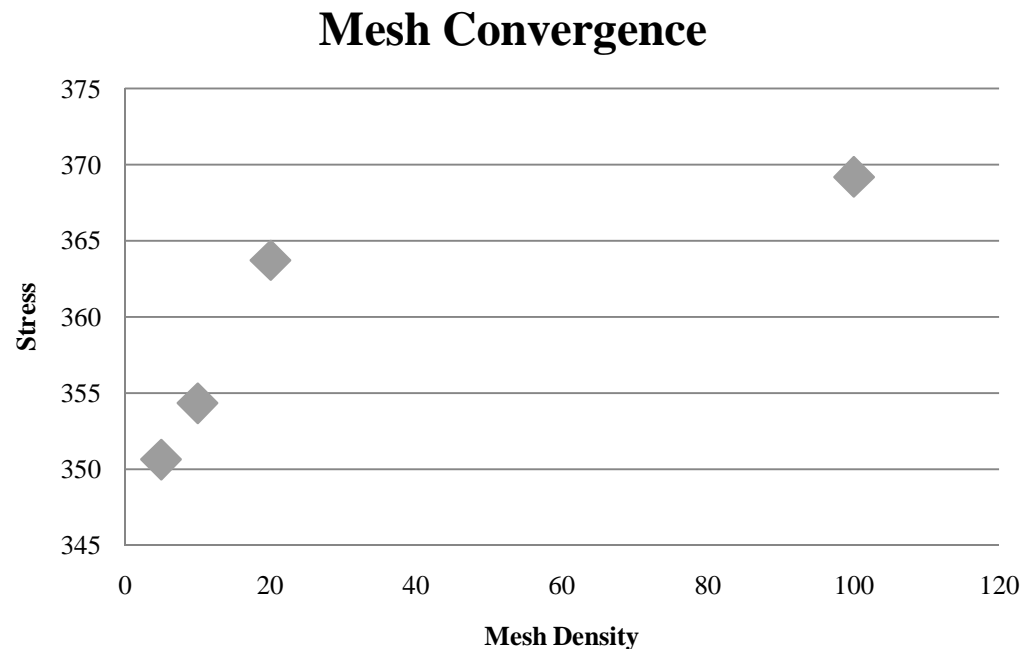
- Stress along path
 - Varying Mesh densities



Case Study B



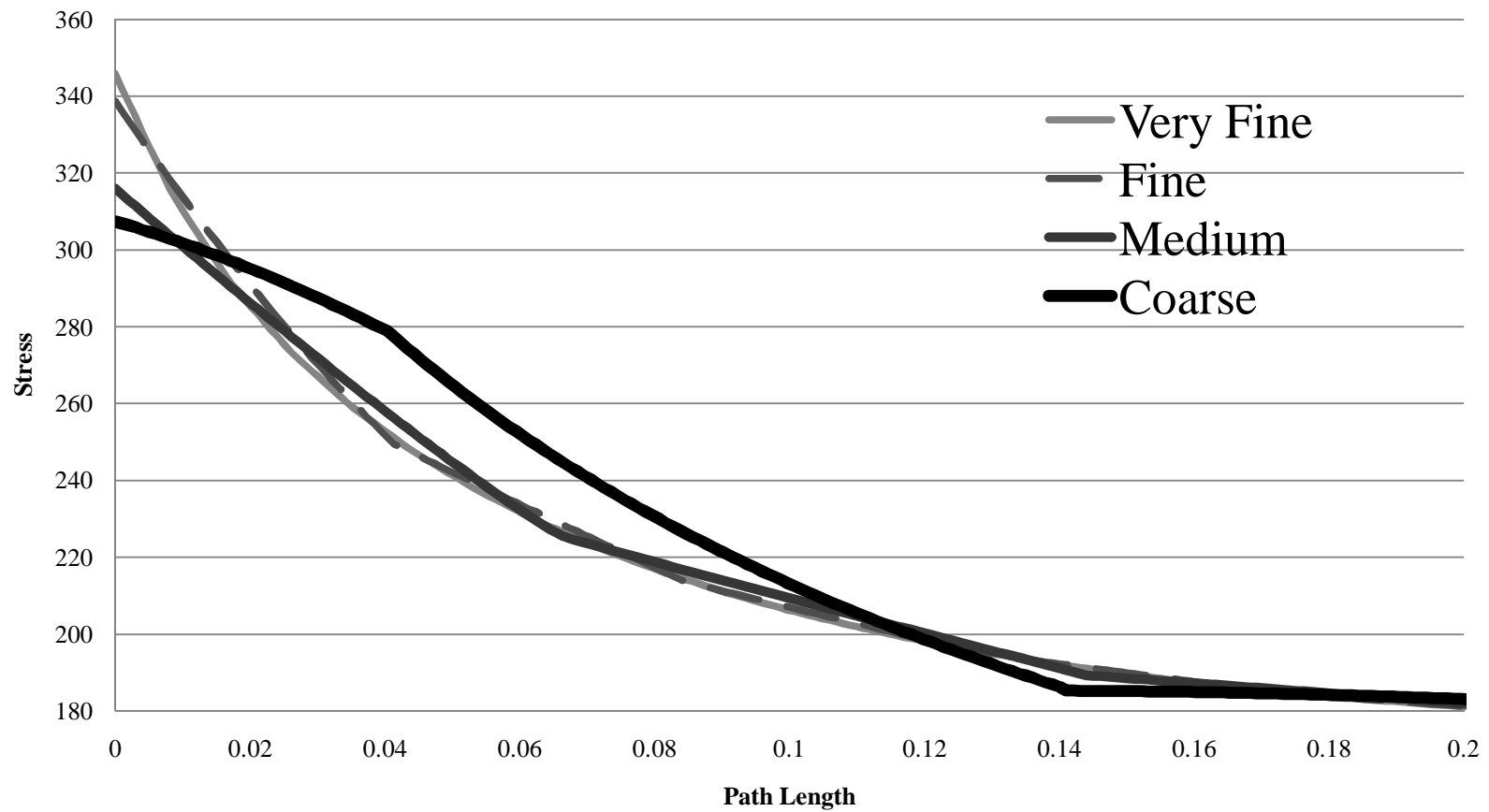
- Peak Stress
 - Varying Mesh densities
 - WB 's adaptive mesh refinement automates this task refining only regions of interest (thanks, paul)



Case Study B



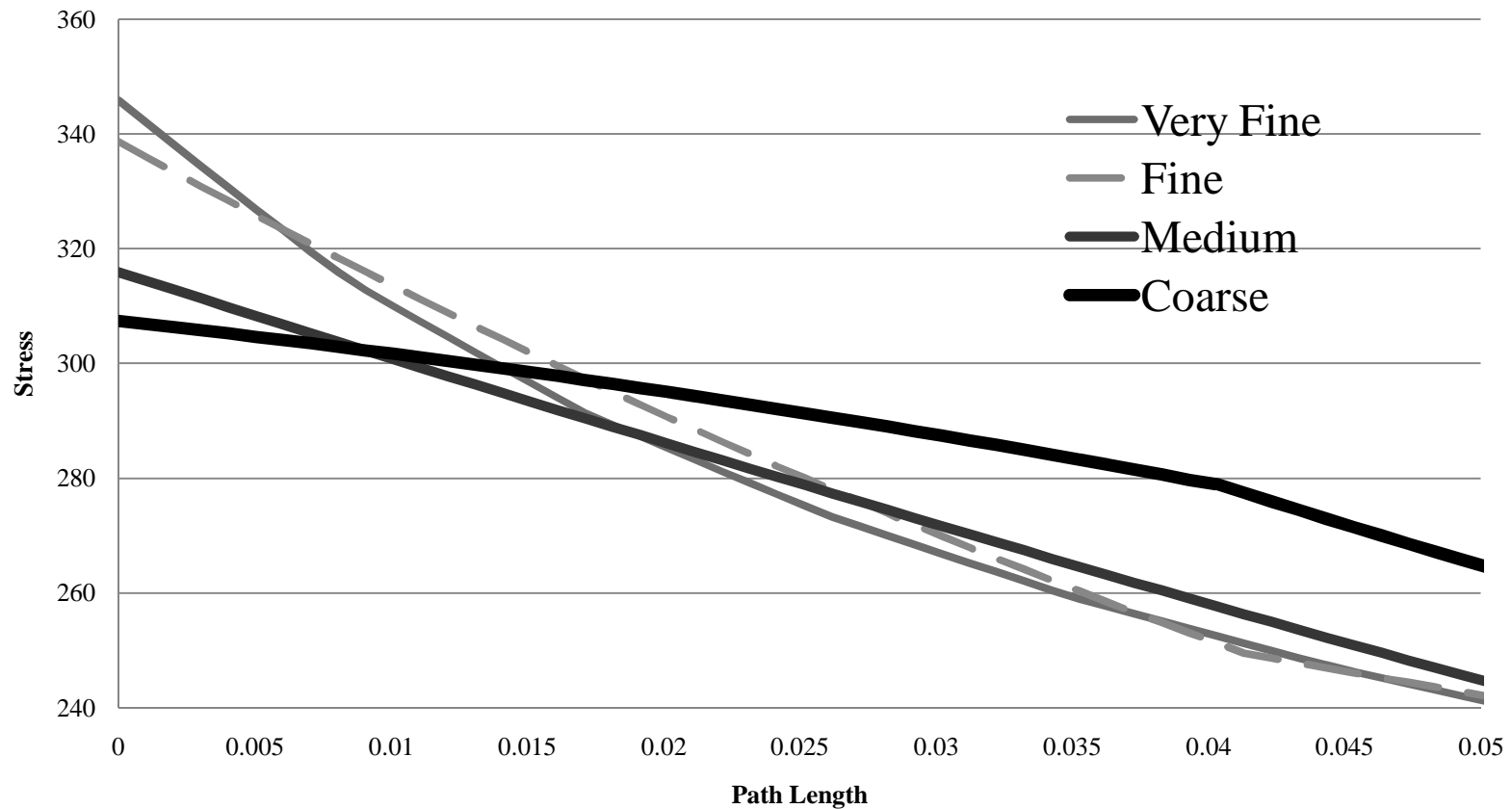
- Stress along path



Case Study B



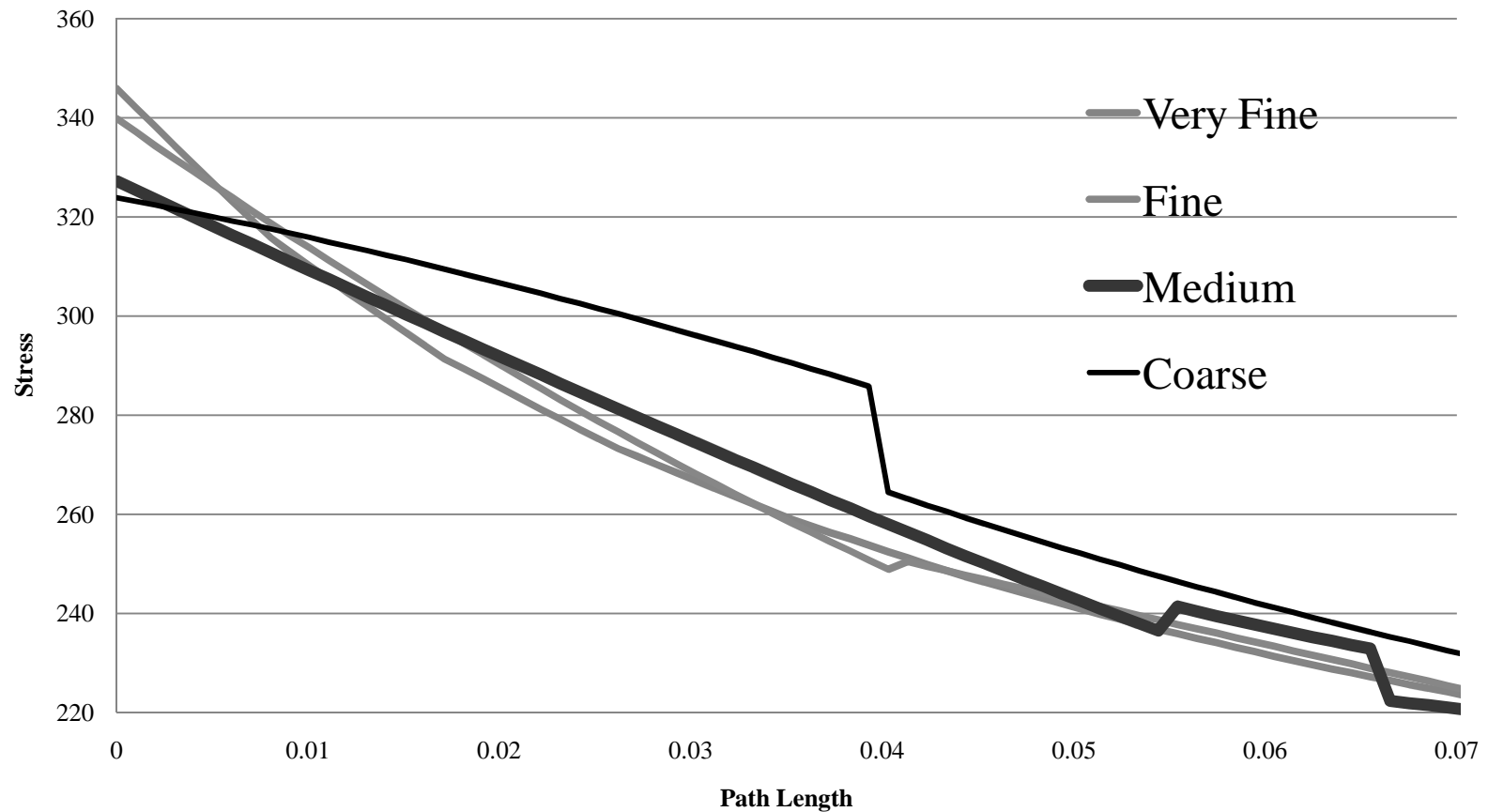
- Stress along path: zoom



Case Study B



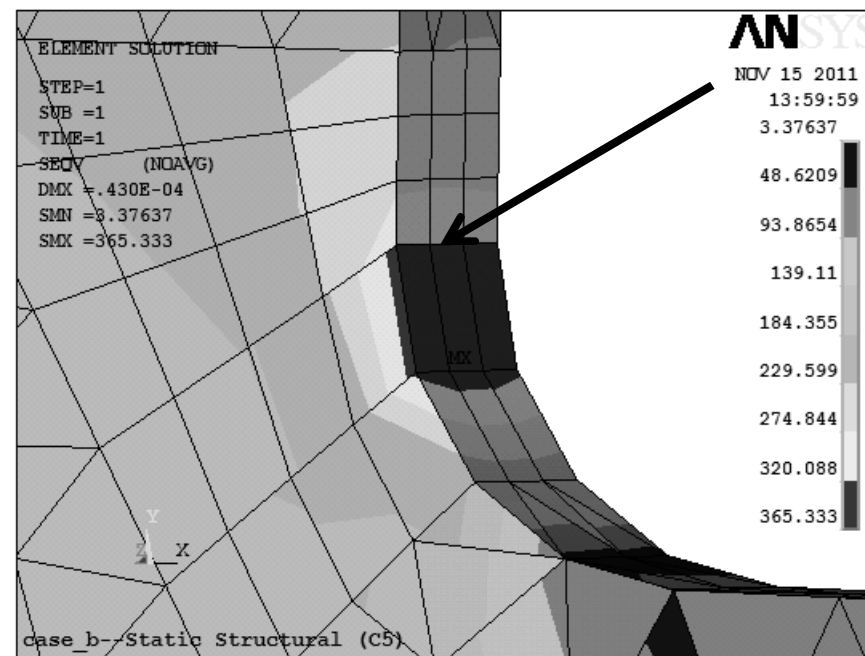
- Stress along path: Unaveraged Results



Case Study B

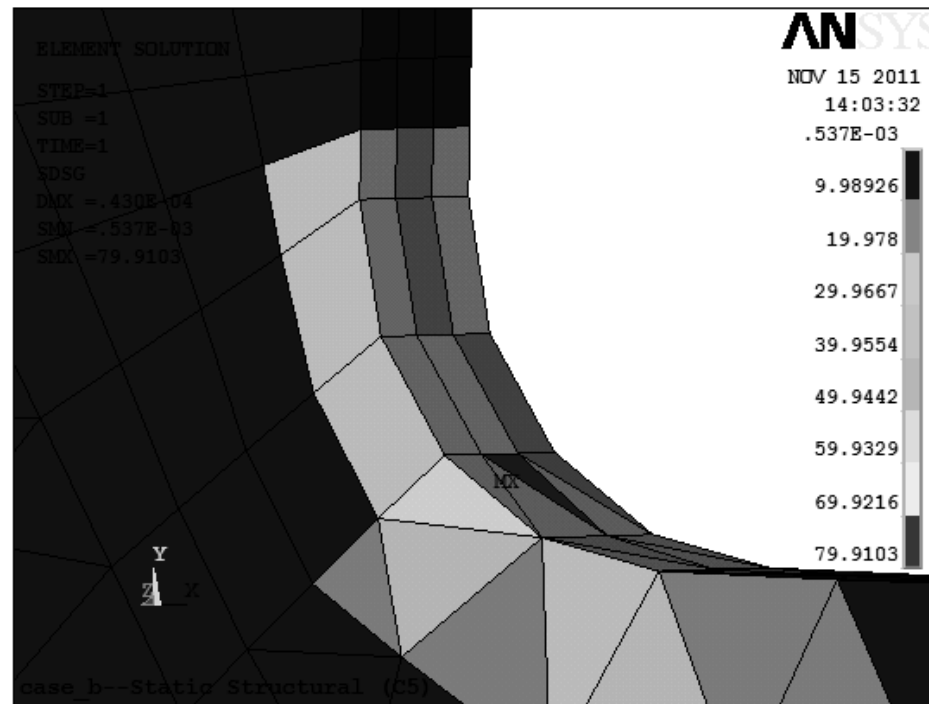


- Case Study B Conclusion:
 - Discontinuity of stress element-to-element relates to degree of mesh discretization error



- Discontinuity at element boundaries is key

$$\{\Delta\sigma_n^i\} = \{\sigma_n^a\} - \{\sigma_n^i\} \quad \text{Difference at boundary}$$



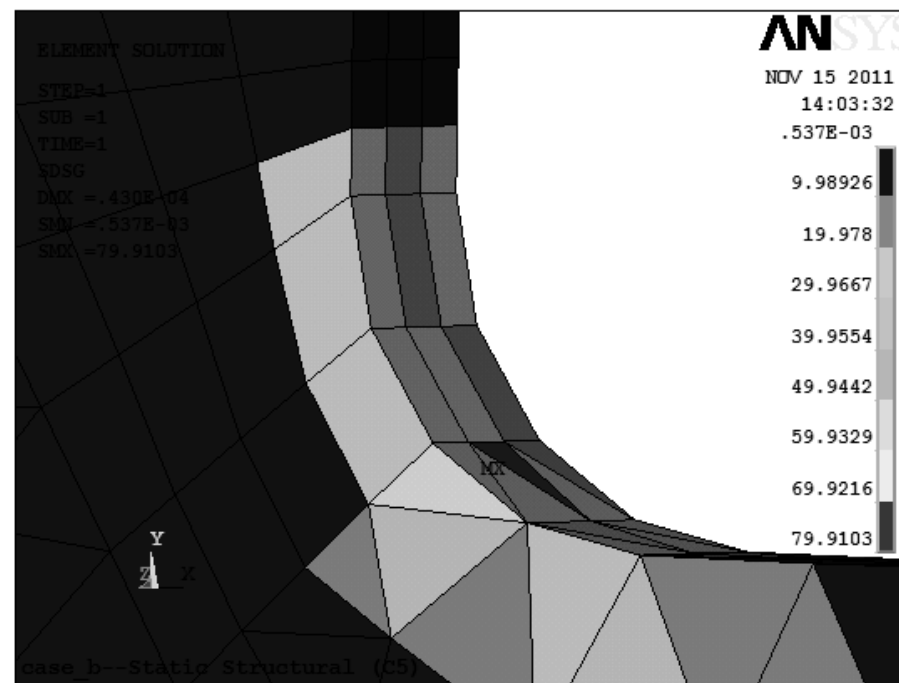
Error Assessment



- Discontinuity at element boundaries is key

$$e_i = \frac{1}{2} \int_{vol} \{\Delta\sigma\}^T [D]^{-1} \{\Delta\sigma\} d(vol)$$

- Energy difference per element
- Considers volume/stiffness



- Discontinuity at element boundaries is key

$$e = \sum_{i=1}^N e_i$$

- Sum it over the model (selected region)

$$E = 100 \left(\frac{e}{U + e} \right)^{\frac{1}{2}}$$

- Normalize it to the whole model energy
(includes load magnitude)

Yields a single number!

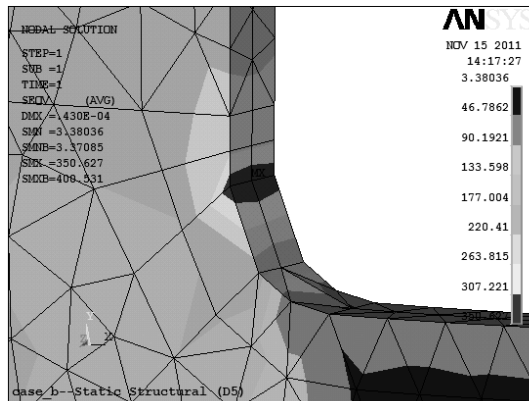
(PRERR, or Percentage error in the energy norm)

Error Assessment



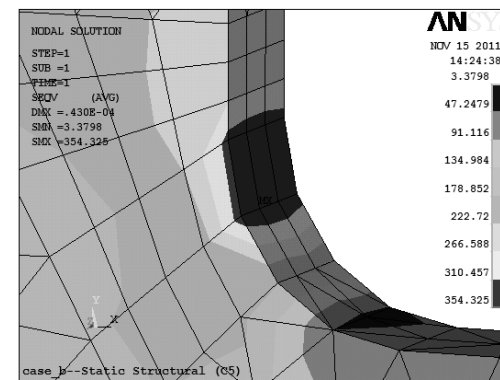
- Percentage error in the energy norm (PRERR)

Coarse

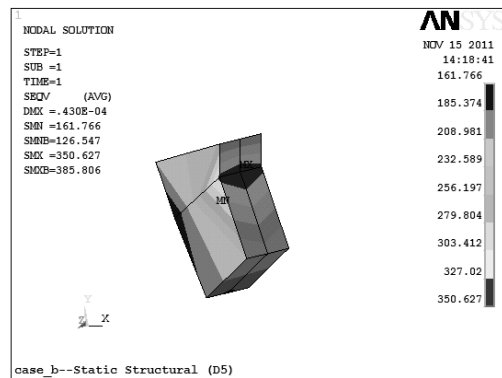


1.59

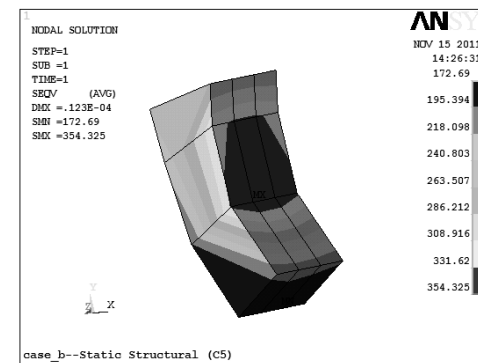
Medium



0.797



8.95



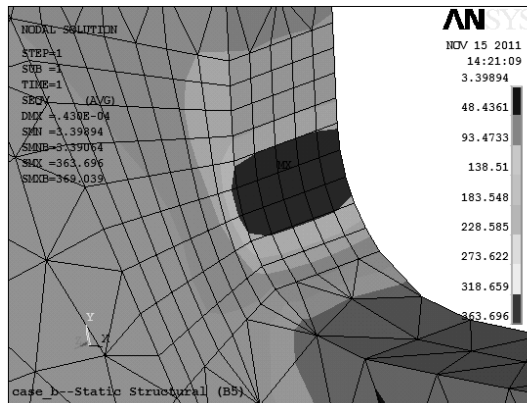
4.0

Error Assessment



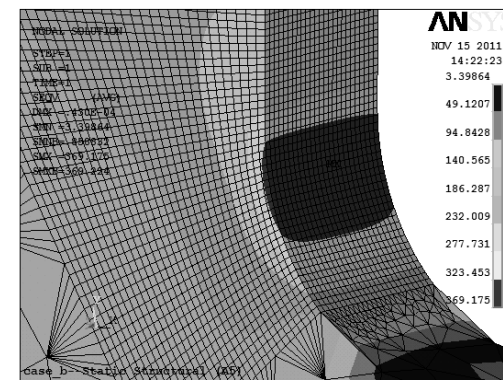
- Percentage error in the energy norm (PRERR)

Fine

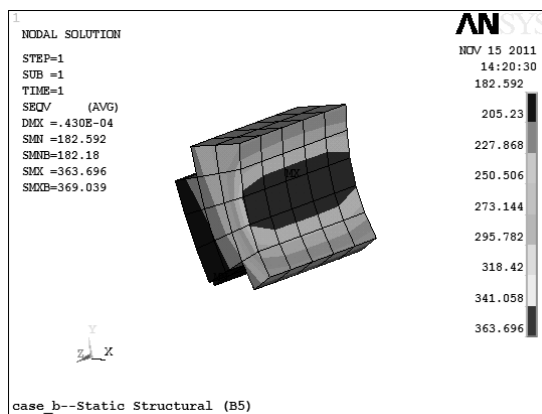


0.56

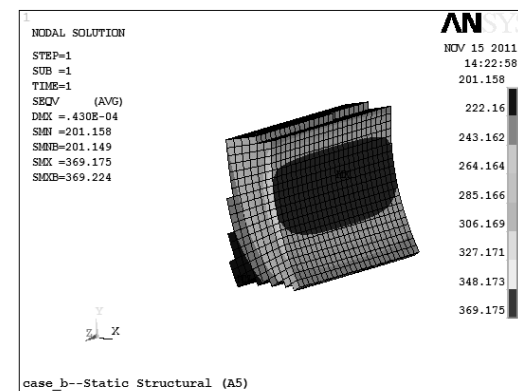
Very Fine



0.32



1.13



0.06

- SMXB

- Checks all nodes (doesn't necessarily correspond to the MX location!)
- Only mentioned once in Help Manual!
- Training Classes refer to it as a “confidence band”...

$$\sigma_j^{mxb} = \max(\sigma_{j,n}^a + \Delta\sigma_n)$$

Root Mean Square of:
(avg. value – element value)
for each element sharing node

Average stress from
contributing elements
(what's plotted)

/EOF